

DESIGN OF RNS FREQUENCY SAMPLING FILTER BANKS

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ABSTRACT

Frequency sampling filters (FSF) are of interest to the designers of multirate filter banks due to their intrinsic low-order, complexity, and linear phase behavior. Fast FSFs residing in smaller packages will be required to support future high-bandwidth, mobile image and signal processing applications. Since FSF designs rely on the exact annihilation of selected poles-zeros, a new facilitating technology is required which is fast, compact, and numerically exact. Exact FSF pole-zero annihilation is guaranteed by implementing polynomial filters over an integer ring in the residue arithmetic system (RNS). The design methodology is evaluated as an ASIC. Based on an FPGA technology, at least an 86% complexity reduction can be achieved with even greater advantages gained as a custom VLSI. An RNS-based FSF implementation of an eight channel cochlea filter bank is presented which demonstrates both the performance and packaging advantages of the new FSF paradigm.

1. INTRODUCTION

A classical frequency sampling filter (FSF) consists of a comb filter cascaded with a bank of frequency selective resonators [1, 2]. The resonators independently produce a collection of poles which annihilate the zeros produced by the comb pre-filter. The gains applied to the output of the resonators are chosen so as to approximately profile the magnitude frequency response of a desired filter. For stability reasons, the poles and zeros are generally designed to be slightly interior to the unit circle. An FSF can also be created by cascading all-pole filter sections with all-zero filter (comb) sections as suggested in Figure 1. The delay of the comb-section $1 \pm z^{-D}$ are chosen that its zeros cancel the poles of the all-pole prefilter as shown in Figure 2. It can be observed that wherever there is a complex pole there also exists an annihilating complex zero which results in an all-zero FIR input-output behavior, with the usual linear phase and constant group delay properties. FSF filters of this type are known to provide very efficient multirate interpolation and decimation solutions as well as serve as high-decimation rate filters for RF to baseband conversion of radio signals [3].

This work was supported by the German DFG under grand ME1419/2-1.

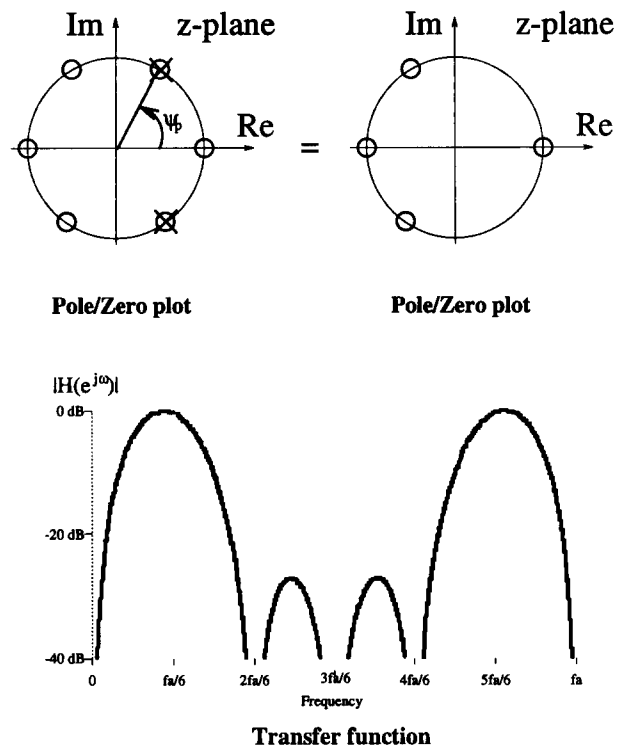


Figure 2: Example of pole/zero-compensation for a pole-angle of 60° and Comb-delay $D = 6$. [4].

2. FREQUENCY SELECTIVE PROPERTIES

The poles of the FSF filter developed in this paper will reside on the periphery of the unit circle. This is in contrast with the customary practice of forcing the poles and zeros to reside at interior locations to guard against possible inexact pole-zero cancellation. It will be shown the stability is not an issue if the FSF is implemented using the exact residue number system (RNS). The RNS [5] is an exact arithmetic system which is also known to possess a bandwidth/area ratio which greatly exceeds that obtainable using conventional fixed-point system (e.g., two's complement) in FIR-like applications, especially when complex arithmetic is performed. Arithmetic in the RNS is performed in a modular sense within a set of relatively-prime, independent, small wordlength channels. An example of an

Table 1: Filters with integer coefficients producing unique angular pole locations up to order six.

$C_k(z)$	Order	a_0	a_1	a_2	a_3	a_4	a_5	a_6	ψ_1	ψ_2	ψ_3
$-C_1(z)$	1	1	-1						0°		
$C_2(z)$	1	1	1						180°		
$C_6(z)$	2	1	-1	1					60°		
$C_4(z)$	2	1	0	1					90°		
$C_3(z)$	2	1	1	1					120°		
$C_{12}(z)$	4	1	0	-1	0	1			30°	150°	
$C_{10}(z)$	4	1	-1	1	-1	1			36°	108°	
$C_8(z)$	4	1	0	0	0	1			45°	135°	
$C_5(z)$	4	1	1	1	1	1			72°	144°	
$C_{16}(z)$	6	1	0	0	-1	0	0	1	20.00°	100.00°	140.00°
$C_{14}(z)$	6	1	-1	1	-1	1	-1	1	25.71°	77.14°	128.57°
$C_7(z)$	6	1	1	1	1	1	1	1	51.42°	102.86°	154.29°
$C_9(z)$	6	1	0	0	1	0	0	1	40.00°	80.00°	160.00°

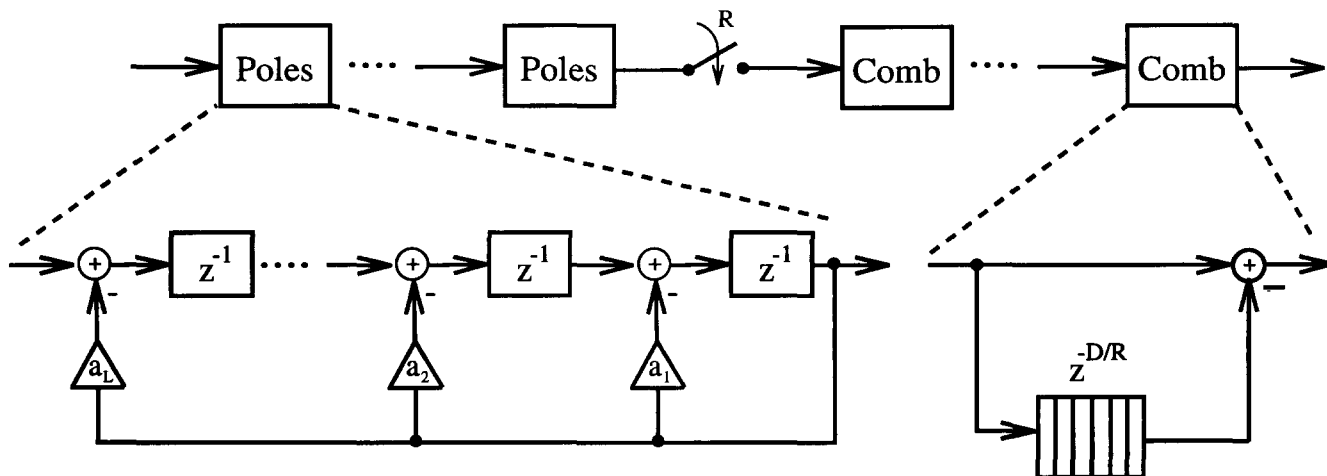


Figure 1: Cascading of frequency sampling filter to save a factor of R delays for multirate signal processing [1, Sec. 3.4].

RNS systolic array of multiply-accumulate (MAC) cells is shown in Figure 3. In addition, by allowing the FSF poles and zeros to reside on the unit circle, a multiplier-less FSF can be realized with an attendant reduction in complexity an increase in data bandwidth.

In Figure 1, first-order filter sections are used to produce poles the angles 0° and 180° (i.e., $z = \pm 1$). Second-order sections with integer coefficients can produce poles at angles 60° , 90° , 120° according to $2 \cos(2\pi K/D) = 1, 0,$ and -1 . For sections of higher order, there are no single frequency selective filters as shown in Table 1. Here the results of complete search are reported for all polynomials up to order six, with integer coefficients and roots on the unit circle which deliver additional (new) angular frequencies. From this list of filters, up to order twenty-four, with integer coefficients and poles residing on the periphery of the unit circle, an efficient and compact FSF can be designed and implemented.

3. CYCLOTOMIC POLYNOMIALS

The integer polynomials from Table 1 found by computer search are known from number theory as cyclotomic polynomials which are defined by [6, p.158-160]:

$$C_k(z) = \prod_{\substack{\gcd(r,k)=1 \\ 0 < r < k}} z - W_k^r \quad (1)$$

where $\gcd(r, k)$ is the greatest common divisor of r and k . A useful property of $C_k(z)$ is that the order of the polynomial is equal to the Euler totient function $\phi(k)$, which is the number of relative primes not exceeding k . Because $\phi(k)$ is an increasing function with a lower bound of $\phi(k) \geq 0.215481 \cdot k^{1.0077} + 1.36$, for all $k > 5$, only cyclotomic polynomials up to $k = 18$ are to be evaluated for polynomials of order six and $k = 30$ for polynomials of order eight, see Figure 4. The $C_k(z)$ were used to verify the results shown in Table 1. It's interesting to notice [7, p.74] that the coefficients of $C_k(z)$, up to $k = 105$, are one of 0,1, or -1 and

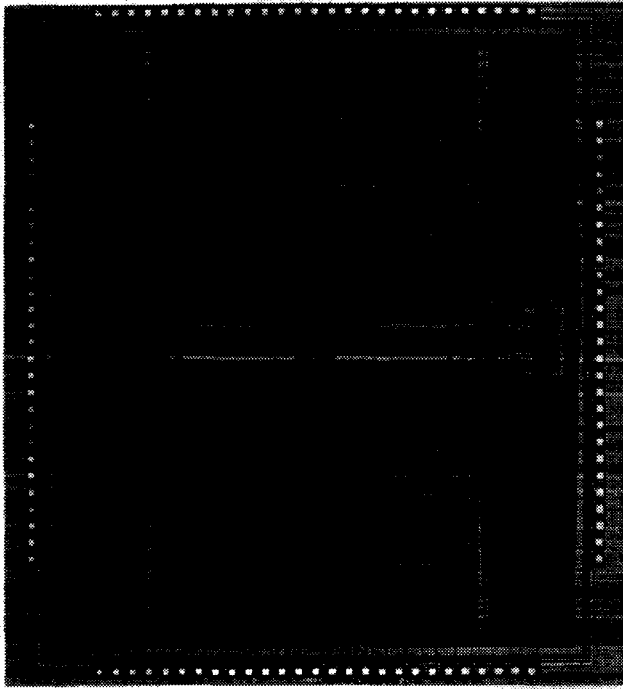


Figure 3: RNS systolic array chip. [4].

only polynomials with order higher than twenty-four have coefficients greater than 1. FSF in the RNS are therefore *multiplier free* up to order twenty-four.

4. DESIGN EXAMPLE

An RNS filter bank, developed for use as a cochlea implant, was designed using a Stanford-Implant eight filter model having logarithmic coverage of the frequency range from 900-8000 Hz [8, 9]. Using the developed design procedure, and a maximal pole positional error criterion of 5.7% (see Table 2) from the Stanford-Implant ideal, a sixth order solu-

Table 2: Error for different maximal order of the pole section.

	mean error	Maximum error
First angle up to order six	3.6%	5.7%
All angle up to order six	2.8%	4.7%
All angle up to order eight	2.4%	3.7%

tion was found at a sampling frequency of 16624 Hz. An integer coefficient half-band filter HB6 [10] anti-aliasing filter and third order multiplier-free CIC-filter (a.k.a. Hogenauer filter [11]), was added to the design to suppress unwanted frequency components as shown in Figure 5. The bandwidth of each resonator can be independently tuned by the number of stages and the delays in the comb-section. The number of stages and delay was optimized to meet the lis-

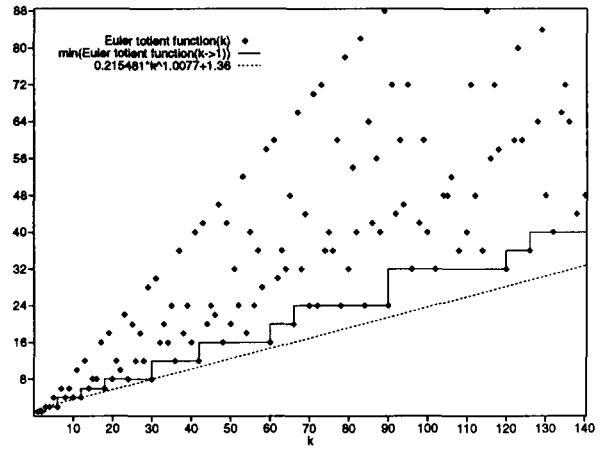


Figure 4: Order of $C_k(z)$, which is $\phi(k)$. Computation of lower bound by starting with a high k value (1000) and computing $\phi(k)$ down to $k = 1$. Lower bound approximation for $k > 5$ is $\phi(k) \geq 0.215481 \cdot k^{1.0077} + 1.36$.

tener bandwidth requirements [12]. All frequency selective filters have two stages and delays.

Table 3: Bit width of the single filter.

Filter	Stage 1	Stage 2	Stage 3	Stage 4
F20	20	17	15	14
F25	20	18	15	14
F36	20	17	15	14
F51	19	16	15	14
F72	20	16	15	14
F90	20	17	15	14
F120	20	17	15	14
F180	19	16	15	14
III	19	18	17	
D4,D5	16	16	15	
HB6	22			

The design was prototyped using Xilinx XC4000 FPGAs with the complexity reported in Table 3 and Table 4. Using high-level design tools, the number of used CLBs is typically 20% more than the theoretical prediction obtained by counting adder, flip-flops, ROMs and RAMs. A custom CMOS RNS design, based on the cells used in the device shown in Figure 3, is being pursued for comparative purposes.

5. CONCLUSION

A methodology for efficiently implementing FSF filters having poles (up to order twenty-four) and zeros on the unit circle is presented. The implementation was based on the use of the exact RNS arithmetic system which insured pole-zero annihilation was complete. The RNS-based FSF processor was studied in the context of an FPGA design, consisting of 1572 CLBs of a Xilinx XC4000 and a custom CMOS device. A custom VLSI device is also being developed to further reduce the complexity of an FSF system. The resulting sys-

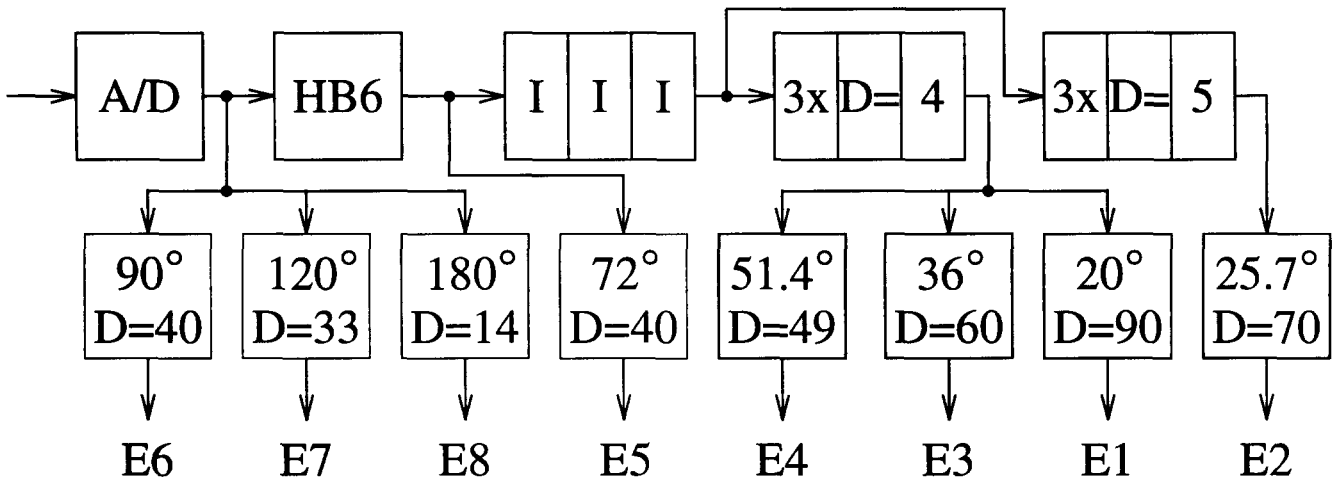


Figure 5: Design of an artificial cochlea consisting of a half-band and CIC prefilter and FSF comb-resonator sections.

Table 4: Number of used CLBs of Xilinx XC4000 FPGAs (Notation: F20D90 means filter pole-angle 20.00° delay Comb $D = 90$). Total Practice: 1572 CLBs. Total non-recursive FIR: 11292 CLBs.

	F20D90	F25D70	F36D60	F51D49
Theory	122	184	128	164
Practice	160	271	190	240
Nonrec.	2256	1836	1924	1140

	F72D40	F90D40	F120D33	F180D14
Theory	124	65	86	35
Practice	190	93	120	53
Nonrec.	1039	1287	1260	550

	HB6	III	D4	D5
Theory	122	31	24	24
Practice	153	36	33	33

tem, compared to conventional implementations, are shown to possess a superior bandwidth/complexity (area) metric which is important in applications having severe packaging constraints (i.e., mobile applications).

6. REFERENCES

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