

Wavelet Transform and its relation to multirate filter banks

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Outline

Short – Time Fourier – Transformation

- Interpretation using Bandpass Filters
- Uniform DFT Bank
- Decimation
- Inverse *STFT* and filter - bank interpretation
- Basis Functions and Orthonormality
- Continuous Time *STFT*

Wavelet – Transformation

- Passing from *STFT* to Wavelets
- General Definition of Wavelets
- Inversion and filter - bank interpretation
- Orthonormal Basis
- Discrete – Time Wavelet Transf.
- Inverse

First, we will develop the short – time Fourier transform (*STFT*) and its relation to filter banks and then the wavelet transform and its relation to multirate filter banks.

Therefore it is much easier to understand, if first the discrete time *STFT* and afterwards the continuous time *STFT* will be introduced. Followed by continuous wavelet transform and discrete wavelet transform.

• SHORT-Time FOURIER TRANSF.

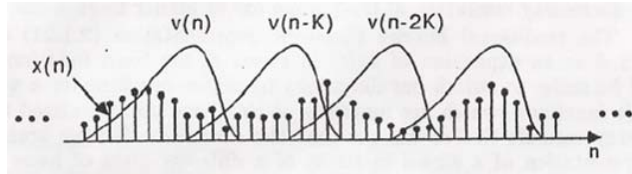


figure 1: STFT processing in time

time – frequency plot = Spectrogram

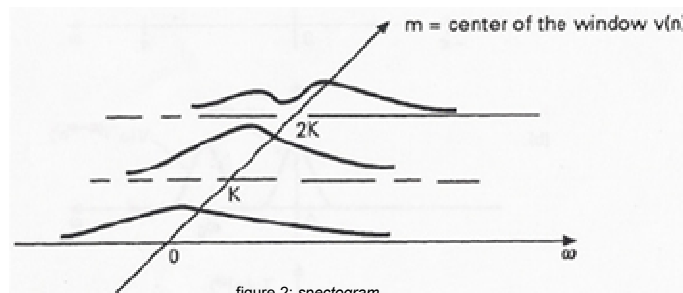


figure 2: spectrogram

In short – time Fourier transform, a signal $x(n)$ is multiplied with a window $v(n)$ (typically finite in duration). \rightarrow The Fourier – transform of the time domain product $x(n)v(n)$ is computed, and then the window is shifted in time, and the FT of the new product computed again. (figure 1)

This operation results in a separate FT for each location m of the center of the window, which is typically an integer multiple of some fixed integer K). (figure 2)

Definition:

$$X_{STFT}(e^{j\omega}, m) = \sum_{n=-\infty}^{\infty} x(n)v(n-m)e^{-j\omega n}$$

m . . . *time shift – variable*

(typically an integer multiple of some fixed integer K)

ω . . . *frequency – variable* $-\pi \leq \omega < \pi$

From above discussion it is clear that the *STFT* can be written mathematically as shown in the slide, where ω is continuous and takes the usual range between $-\pi$ and $+\pi$.

- *Interpretation using Bandpass Filters*

Traditional Fourier Transform as a Filter Bank

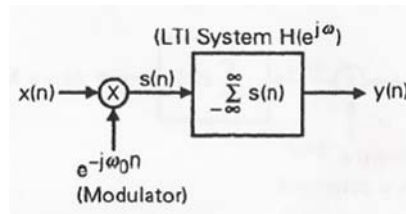


figure 3: Representation of FT in terms of a linear system

1. *Modulator* $e^{-j\omega_0 n}$: \rightarrow *performs a frequency shift*
2. *LTI – System* $H(e^{j\omega})$: \rightarrow *ideal lowpass filter*

Before interpreting the *STFT* in terms of filter banks, we will begin by representing a filter bank interpretation for the traditional Fourier – Transform. (figure 3)

\rightarrow Figure 3 represents only one channel for one specific frequency ω_0 .

Why is $H(e^{j\omega})$ an ideal lowpass filter ?

Impulse Response $h(n) = 1$ for all n

$$\rightarrow H(e^{j\omega}) = \sum_{n=-\infty}^{\infty} h(n)e^{-j\omega n} = 2\pi\delta_a(\omega) \quad -\pi \leq \omega < \pi$$

→ only zero - frequency passes

→ every other frequency is completely suppressed

$$y(n) = X(e^{j\omega_0}) \quad \text{for all } n$$

$h(n) = 1$ for all n . This system is evidently unstable, but let us ignore these fine details for the moment.

$\delta_a(\omega)$ is the Dirac delta function.

Summarizing, the process of evaluating $y(n) = X(e^{j\omega_0})$ can be looked upon as a linear system, which takes the input $x(n)$ and produces a *constant* output $y(n)$.

Therefore, the FT operator is a bank of modulators followed by filters. This system has an uncountably infinite number of channels.

STFT as a Bank of Filters

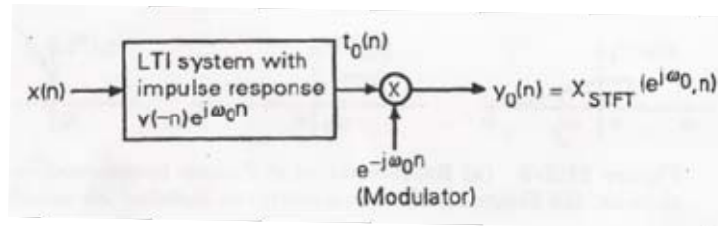
→ Expansion of Definiton for further insight!

$$X_{STFT}(e^{j\omega}, m) = e^{-j\omega m} \sum_{n=-\infty}^{\infty} x(n) v(n-m) e^{j\omega(m-n)}$$

with:

$$v(n-m) e^{j\omega(m-n)} = v(-(m-n)) e^{j\omega(m-n)}$$

→ Convolution of $x(n)$ with the impulse response of the LTI – System $v(-n) e^{j\omega n}$

figure 4: Representation of *STFT* in terms of a linear system

In most applications, $v(n)$ has a lowpass transform $V(e^{j\omega})$.

→

$$v(-n) \xrightarrow{\circ} V(e^{-j\omega})$$

$$v(-n)e^{j\omega_0 n} \xrightarrow{\circ} V(e^{-j(\omega-\omega_0)})$$

Figure 4 shows the interpretation of the *STFT* in terms of a filter bank. (Again, only one channel can be seen).

The first is an LTI filter followed by the modulator.

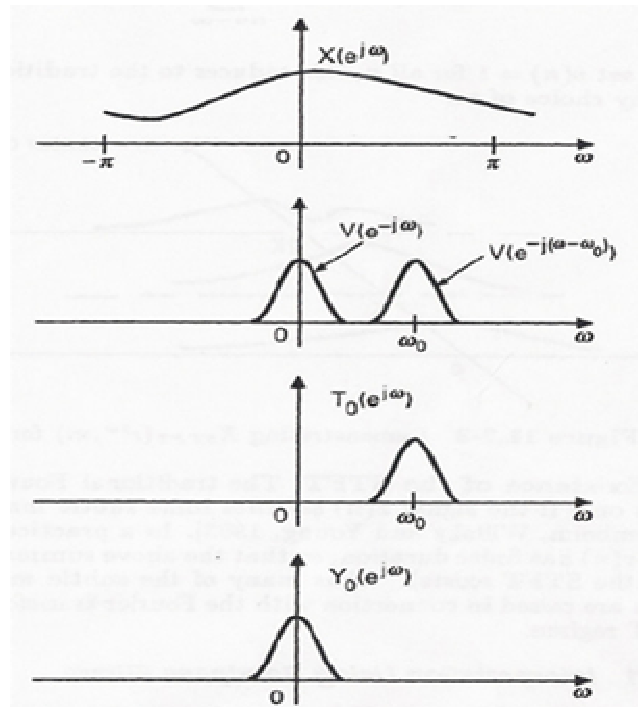
figure 5: Demonstration of how *STFT* works

Figure 5 demonstrates how the *STFT* works.

- (a) FT of an arbitrary chosen input signal $x(n)$
- (b) the window – transform and its shifted version
- (c) output of LTI filter
- (d) traditional Fourier transform of $X_{STFT}(e^{j\omega_0}, n)$

Hence, the *STFT* can be looked upon as a filter bank, with *infinite* number of filters (one per frequency) !

In practice, we are interested in computing the Fourier transform at a discrete set of frequencies

$$\rightarrow 0 \leq \omega_0 < \omega_1 < \dots < \omega_{M-1} < 2\pi$$

Therefore the STFT reduces to a filter bank with M bandpass filters

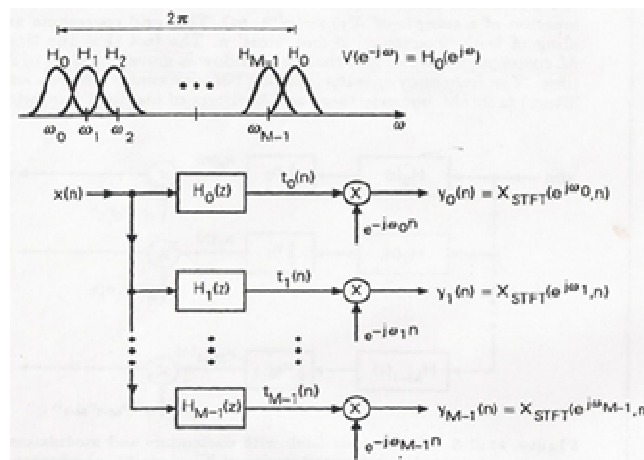


figure 6: STFT viewed as a filter bank

Uniform DFT bank

If the frequencies ω_k are uniformly spaced, then the system becomes the uniform DFT bank.

The M filters are related as in the following manner

$$H_k(z) = H_0(zW^k) \quad 0 \leq k \leq M-1 \quad W = e^{-j\frac{2\pi}{M}}$$

$$\rightarrow H_k(e^{j\omega}) = H_0\left(e^{j(\omega - \frac{2\pi}{M}k)}\right) \quad H_0(e^{j\omega}) = V(e^{-j\omega})$$

→ The *uniform DFT bank* is a device to compute the *STFT* at uniformly spaced frequencies.

→ The frequency responses $H_k(e^{j\omega})$ are uniformly shifted versions of $H_0(e^{j\omega})$

Decimation

if passband width of $V(e^{j\omega})$ is narrow

→ output signals $y_k(n)$ are *narrowband lowpass signals*

this means, that $y_k(n)$ varies slowly with time

According to this varying nature, one can exploit that to decimate the output.

Decimation Ratio of M = moving the window $v(k)$ by M samples at a time

if filters have *equal* bandwidth

→ $n_k = M$

→ *maximally decimated* analyses bank

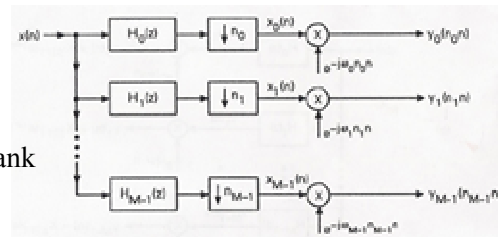


figure 7: Analysis bank with decimators

Figure 7 shows a decimated *STFT* system, where the modulators have been moved past the decimators.

In a more general system n_k could be different for different k , and moreover $H_k(z)$ may not be derived from one prototype by modulation. Such a system, however, does not represent the *STFT* obtainable by moving a single window across the data $x(n)$. → this systems will be admitted in the wavelet transform.

Time – Frequency Grid

Uniform sampling of both, 'time' n and 'frequency' ω

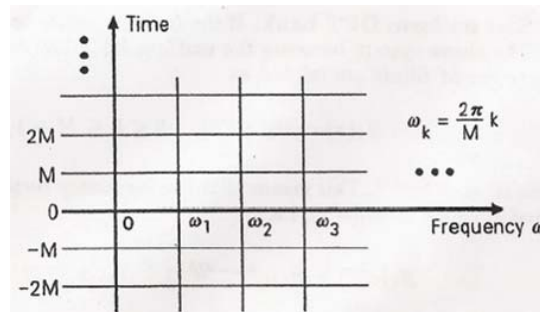


figure 8: time – frequency grid

Time spacing M corresponds to moving the window M units (= samples) at a *time*.

$$\text{frequency spacing of adjacent filters} = \frac{2\pi}{M}$$

Inversion of the STFT

From traditional Fourier – viewpoint

$X_{STFT}(e^{j\omega}, m)$ is the FT. from the time domain product
 $x(n)v(n-m)$

$$\rightarrow x(n)v(n-m) = \frac{1}{2\pi} \int_0^{2\pi} X_{STFT}(e^{j\omega}, m) e^{j\omega n} d\omega$$

For example, if we set $n = m$ we obtain the *STFT* inversion formula for $x(m)$ as long as $v(0)$ exists. If it does not, we can pick some other value of m .

Another inversion formula is given by:

$$x(n) = \frac{1}{2\pi} \int_0^{2\pi} \left(\sum_{m=-\infty}^{\infty} X_{STFT}(e^{j\omega}, m) v^*(n-m) \right) e^{j\omega n} d\omega$$

which is provided by $\sum_m |v(m)|^2 = 1$

if $\sum_m |v(m)|^2 \neq 1$ but finite \rightarrow divide right side of the formula by $\sum_m |v(m)|^2$

but if window energy is infinite \rightarrow one cannot apply this formulation

Filter Bank Interpretation of the Inverse

With $F_k(z)$ as synthesis - filter

Reconstruction can be done by the following synthesis bank:

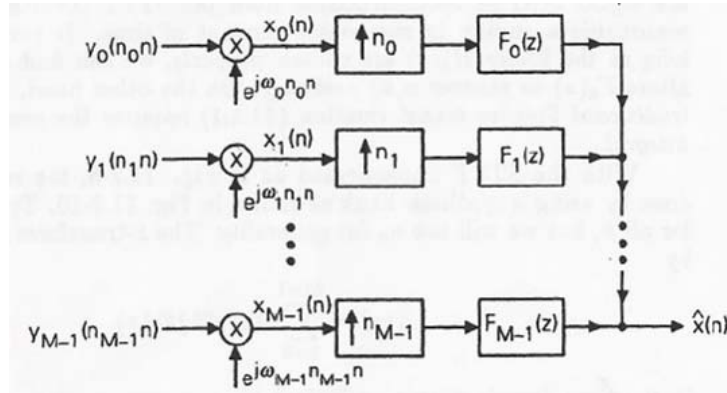


figure 9: synthesis – bank used to reconstruct $x(n)$

typically $n_k = M$ for all k

The z – Transformation of $\hat{x}(n)$ is given by

$$\hat{X}(z) = \sum_{k=0}^{M-1} X_k(z^{n_k}) F_k(z)$$

in time – domain

$$\begin{aligned} \hat{x}(n) &= \sum_{k=0}^{M-1} \sum_{m=-\infty}^{\infty} x_k(m) f_k(n - n_k m) \\ &= \sum_{k=0}^{M-1} \sum_{m=-\infty}^{\infty} y_k(n_k m) e^{j\omega_k(n_k m)} f_k(n - n_k m) \\ &= y_k(n_k m) \dots \text{STFT - Coefficients} \end{aligned}$$

Reconstruction is stable, if the filters $F_k(z)$ are stable!

Perfect reconstruction will be obtained, if $\hat{x}(n) = x(n)$

Basis Functions and Orthonormality

Functions of interest

$$\eta_{km}(n) \triangleq f_k(n - n_k m) \dots \text{basis functions}$$

For these double indexed functions (*basis functions* $\{\eta_{km}(n)\}$),
the orthonormality property means that

$$\sum_{n=-\infty}^{\infty} f_{k1}^*(n - n_{k1} m_1) f_{k2}(n - n_{k2} m_2) = \delta(k_1 - k_2) \delta(m_1 - m_2)$$

should be zero, except for those cases where $k_1 = k_2$ and $m_1 = m_2$

Remember: $k \dots$ filter number $m \dots$ time shift

How should we design the filters $F_k(z)$ in order to ensure this orthonormality property ?

Therefore, the paraunitary property of the polyphase matrix is sufficient!

The Continuous - Time Case

Main points:

$$X_{STFT}(j\Omega, \tau) = \int_{-\infty}^{\infty} x(t)v(t-\tau)e^{-j\Omega t} dt \quad (STFT)$$

$$x(t)v(t-\tau) = \frac{1}{2\pi} \int_{-\infty}^{\infty} X_{STFT}(j\Omega, \tau)e^{j\Omega t} d\Omega \quad (inv. STFT)$$

$$x(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \left(\int_{-\infty}^{\infty} X_{STFT}(j\Omega, \tau)v^*(t-\tau)d\tau \right) e^{j\Omega t} d\Omega \quad (inv. STFT)$$

Because of the close resemblance to the discrete – time case, we only summarize the main points for the continuous – time case.

Historically, the *STFT* was first developed for the continuous – time case by Dennis Gabor.

Choice of “Best Window”

R_{oot} M_{ean} S_{quare} duration of window function $v(t)$ in

time domain D_t

$$D_t^2 = \frac{1}{E} \int_{-\infty}^{\infty} t^2 v^2(t) dt$$

frequency domain D_f

$$D_f^2 = \frac{1}{2\pi E} \int_{-\infty}^{\infty} \Omega^2 |V(j\Omega)|^2 d\Omega$$

with:

$$E \dots \text{window energy } E = \int v^2(t) dt$$

Uncertainty principle:

$$D_t D_f \geq 0.5$$

Iff Gaussian – window, this inequality becomes an equality !

D_t is the rms time domain duration and D_f the rms frequency domain duration of the window.

Filter Bank Interpretation

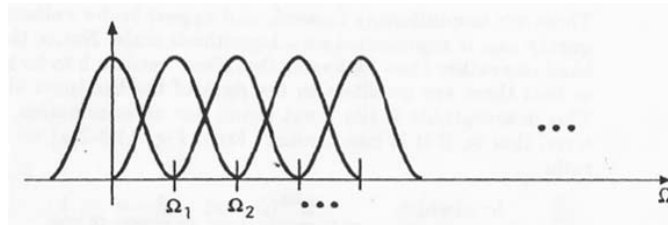
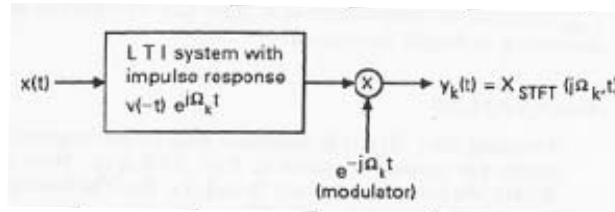


figure 10: continuous – STFT

Figure 10 shows again the filtering interpretation for the continuous – time *STFT*.

● THE WAVELET TRANSFORM

Disadvantage of STFT

uniform time – frequency box ($D_t = \text{const.}$, $D_f = \text{const.}$)

→ The accuracy of the estimate of the Fourier transform
is poor at low frequencies, and improves as the frequency increases.

⇒ *Expected properties for a new function:*

- window width should adjust itself with 'frequency'
- as the window gets wider in time, also the step sizes for moving the window should become wider.

These goals are nicely accomplished by the **wavelet transform**.

Passing from STFT to Wavelets

Step 1:

Giving up the *STFT* modulation scheme and obtain filters

$$h_k(t) = a^{-k/2} h(a^{-k}t) \quad a > 1 \dots \text{scaling factor, } k = \text{integer}$$

in the frequency domain:

$$H_k(j\Omega) = a^{k/2} H(ja^k\Omega)$$

→ all responses are obtained by *frequency – scaling* of a prototype response $H(j\Omega)$

This is unlike the case of *STFT*, where all filters were obtained by *frequency – shift* of a prototype.

The scale factor $a^{-k/2}$ is meant to ensure that the energy $\int_{-\infty}^{\infty} |h_k(t)|^2 dt$ is independent of k .

Example:

Assuming $H(j\Omega)$ is a bandpass with cutoff frequencies α and β .

Also $a = 2$, $\beta = 2\alpha$ and the center frequency should be the geometrical mean of the two cutoff edges

$$\Omega_k = 2^{-k} \sqrt{\alpha\beta} = \alpha 2^{-k} \sqrt{2}$$

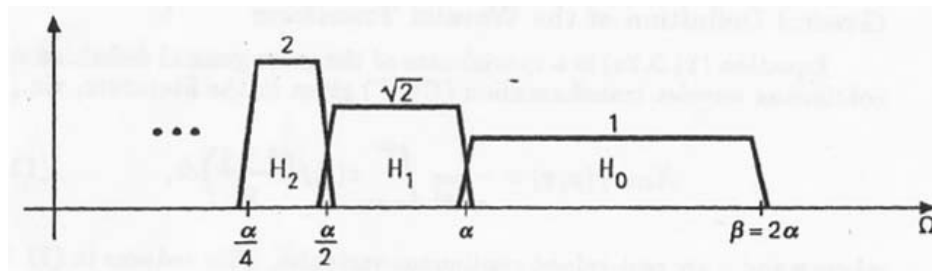


figure 11: frequency – response obtained by scaling process

Ratio:

$$\frac{\text{bandwidth}}{\text{center - frequency } \Omega_k} = \frac{2^{-k}(\beta - \alpha)}{2^{-k} \sqrt{\alpha\beta}} = \frac{1}{\sqrt{2}}$$

is independent of integer k

In *electrical filter theory* such a system is often said to be a 'constant Q' system!

$$(Q \dots \text{Quality factor } Q = \frac{\text{center - frequency}}{\text{bandwidth}})$$

→ filter outputs can be obtained by:

$$a^{-k/2} e^{-j\Omega_k \tau} \int_{-\infty}^{\infty} x(t) h(a^{-k}(\tau - t)) dt$$

Step 2:

$k \uparrow \rightarrow \text{bandwidth of } H_k(j\Omega) \downarrow \rightarrow \text{Samplerate} \downarrow$

or in *time* domain

$k \uparrow \rightarrow \text{window length} \uparrow \rightarrow \text{step size} \uparrow$

Since the bandwidth of $H_k(j\Omega)$ is smaller for larger k , we can sample its output at a correspondingly lower rate. → Viewed in time domain, the width of $h_k(t)$ is larger so that we can afford to move the window by a larger step size!

Therefore:

$$\tau = na^k T \quad n \dots \text{integer}, \quad a^k T \dots \text{step size}$$

hence:

$$h(a^{-k}(na^k T - t)) = h(nT - a^{-k}t)$$

Summarizing, we are computing:

$$X_{DWT}(k, n) = a^{-k/2} \int_{-\infty}^{\infty} x(t) h(nT - a^{-k}t) dt$$

$$\rightarrow$$

$$X_{DWT}(k, n) = \int_{-\infty}^{\infty} x(t) h_k(na^k T - t) dt$$

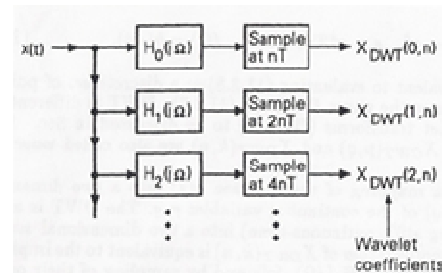


figure 12: Analysis bank of DWT

DWT...Discrete Wavelet Transform

This can be done by replacing the continuous variable τ as shown in the slide.

The modulation factor $e^{-j\Omega_k \tau}$ has been omitted.

What we can see is, that the above integral represents the convolution between $x(t)$ and $h_k(t)$, evaluated at a discrete set of points $na^k T$. In other words, the output of the convolution is sampled with spacing $a^k T$. (figure 12 is a schematic of this for $a = 2$).

Time Frequency Grid

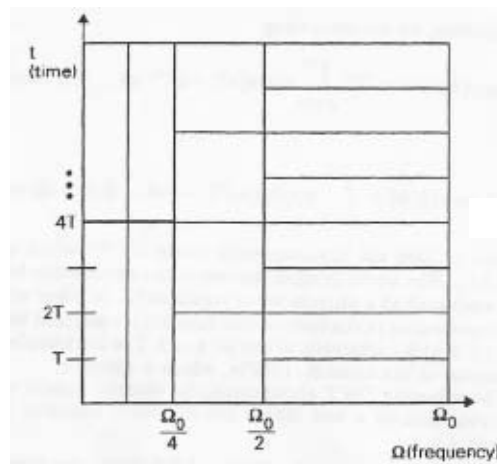


figure 13: time – frequency grid

$$D_t D_f = \text{const.}$$

Frequency spacing is smaller at low frequencies, and the corresponding time – spacing is larger.

General Definition of the Wavelet Transform

$$X_{CWT}(p, q) = \frac{1}{\sqrt{|p|}} \int_{-\infty}^{\infty} x(t) f\left(\frac{t-q}{p}\right) dt$$

p, q ... real – valued continuous variables

According to former definition:

$$p = a^k \quad q = a^k T n \quad f(t) = h(-t)$$

$X_{CWT}(p, q)$ and $X_{DWT}(k, n)$ wavelet coefficients

Inversion of Wavelet Transform

$$x(t) = \sum_k \sum_n X_{DWT}(k, n) \psi_{kn}(t)$$

where $\psi_{kn}(t)$ are the basis functions

Filter Bank Interpretation of Inversion

Reconstruction of $x(t)$ as a designing problem of the following synthesis filter bank

$X_{DWT}(k, n)$... sequence

$F_k(j\Omega)$... continuous in time

→ output of synthesis filter bank :

$$\hat{x}(t) = \sum_k \sum_n X_{DWT}(k, n) f_k(t - a^k nT)$$

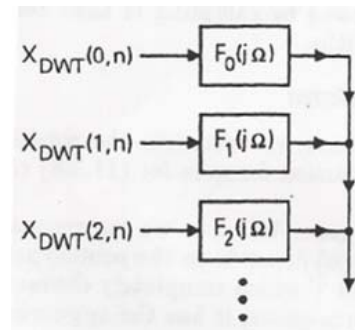


figure 14: synthesis bank

Figure 14 shows the synthesis filter bank.

We have to be careful with the interpretation of this figure. Since $X_{DWT}(k, n)$ is a *sequence*, the signal which is input to the *continuous-time* filter $F_k(j\Omega)$ is actually an impulse train.

All synthesis filters are again generated from a fixed prototype synthesis filter $f(t)$ (\rightarrow *mother wavelet*)

$$f_k(t) = a^{-k/2} f(a^{-k}t)$$

Substituting this in the preceding equation and assuming perfect reconstruction, we get

$$x(t) = \sum_k \sum_n X_{DWT}(k, n) a^{-k/2} f(a^{-k}t - nT)$$

with:

$$\psi(t) = f(t) \rightarrow \psi_{kn}(t) = a^{-k/2} \psi(a^{-k}t - nT) = a^{-k/2} \psi[a^{-k}(t - na^kT)] \dots \text{set of basis functions}$$

using this, we can express each basis function in terms of the filter $f_k(t)$

$$\psi_{kn}(t) = f_k(t - na^kT)$$

Orthonormal Basis

Of particular interest is the case where $\{\psi_{kn}(t)\}$ is a set of orthonormal functions

Therefore, we expect:

$$\int_{-\infty}^{\infty} \psi_{kn}^*(t) \psi_{lm}(t) dt = \delta(k-l) \delta(n-m)$$

using Parseval's theorem, this becomes

$$\frac{1}{2\pi} \int_{-\infty}^{\infty} \Psi_{kn}^*(j\Omega) \Psi_{lm}(j\Omega) d\Omega = \delta(k-l) \delta(n-m)$$

and get :

$$X_{DWT}(k, n) = \int_{-\infty}^{\infty} x(t) \psi_{kn}^*(t) dt$$

Comparing these results, we can conclude:

$$\psi_{kn}(t) = h_k^*(a^k nT - t)$$

And in particular for $k = 0$ and $n = 0$:

$$\psi_{00}(t) = \psi(t) = h^*(-t) \rightarrow \text{for the orthonormal case} \rightarrow f_k(t) = h_k^*(-t)$$

Discrete - Time Wavelet Transform

Starting with the frequency domain relation and a scaling factor $a = 2$

$$H_k(e^{j\omega}) = H(e^{j2^k \omega}) \quad \dots \quad k \text{ is a nonnegative integer}$$

for highpass $H(e^{j\omega})$ and $k = 1, k = 2$

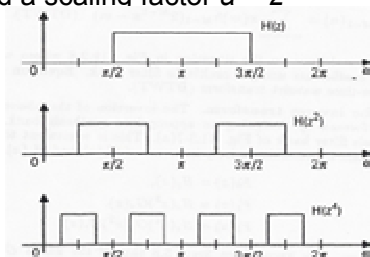
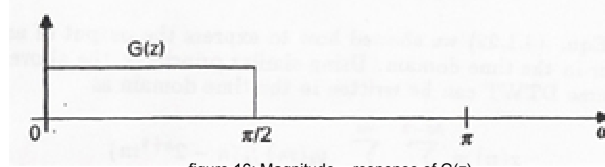


figure 15: Magnitude responses

Let $G(z)$ be a lowpass with response

figure 16: Magnitude – response of $G(z)$

Using QMF – banks

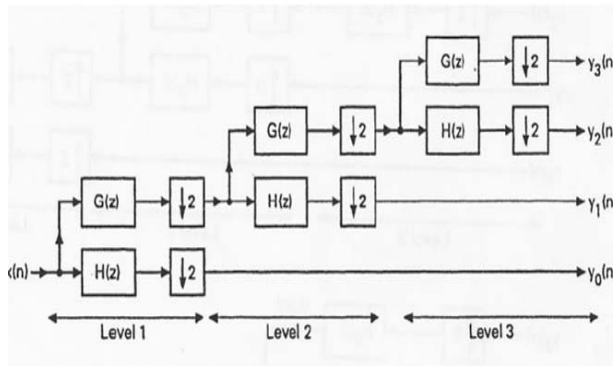


figure 17: 3 level binary tree-structured QMF

or its equivalent

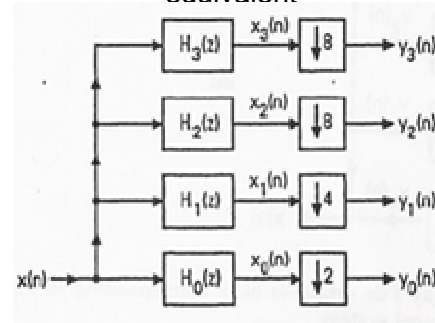
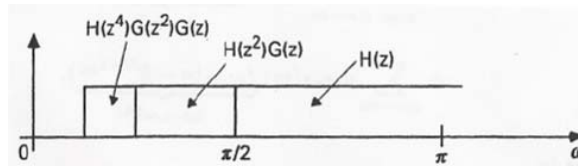


figure 18: equivalent 4-channel system

Responses of the filters $H(z), G(z)H(z^2), G(z)G(z^2)H(z^4), \dots$

figure 19: combinations of $H(z)$ and $G(z)$

Defining the Discrete -Time Wavelet Transform

$$y_k(n) = \sum_{m=-\infty}^{\infty} x(m) h_k(2^{k+1}n - m), \quad 0 \leq k \leq M-2$$

$$y_{M-1}(n) = \sum_{m=-\infty}^{\infty} x(m) h_{M-1}(2^{M-1}n - m), \quad (D_{\text{iscrete}} T_{\text{ime}} WT)$$

Inverse Transform

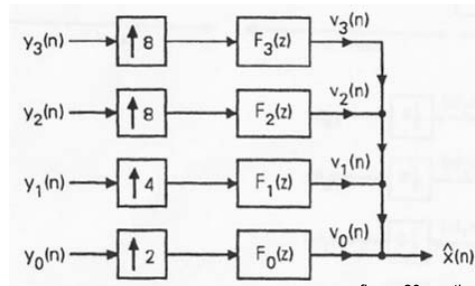
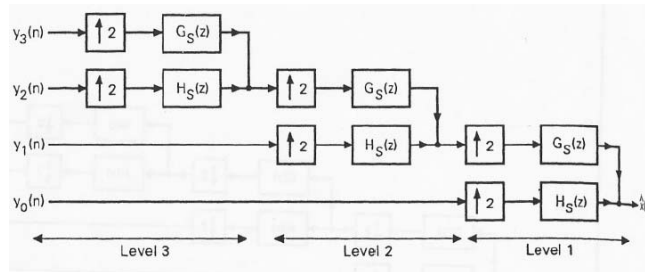


figure 20: synthesis filters

$$F_0(z) = H_s(z), \quad F_1(z) = H_s(z^2)G_s(z), \quad \dots$$

For perfect reconstruction $\hat{x}(n) = x(n)$ we can express

$$X(z) = F_0(z)Y_0(z^2) + F_1(z)Y_1(z^4) + \dots + F_{M-2}(z)Y_{M-2}(z^{2^{M-1}}) + F_{M-1}(z)Y_{M-1}(z^{2^{M-1}})$$

and in time domain:

$$x(n) = \sum_{k=0}^{M-2} \sum_{m=-\infty}^{\infty} y_k(m) f_k(n - 2^{k+1}m) + \sum_{m=-\infty}^{\infty} y_{M-1}(m) f_{M-1}(n - 2^{M-1}m)$$

Main References

Multirate Systems and Filter Banks

(Prentice Hall Signal Processing Series)

by *P. P. Vaidyanathan*